# Enhancement of Visible Light Backscatter Communication by Optimally Locating the Tags

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Abstract—The visible light backscatter communication system has the advantages of sniffing and biological friendliness over the conventional radio frequency (RF) range one, which is essential in indoor communication. In this paper, we focus on the global optimally locating the tag to maximize the effective signal-noise ratio (SNR) in both the single-tag and the two-tags models. Closed-form expressions for the global-optimal locations of the tag are obtained for both two models by using the proposed novel expression of the effective SNR which includes consideration of physical blocking by tags and the optimization of time allocated to each tag for backscattering. Numerical results show that in one tag model, the optimized location of the tag should be placed close to the transmitter. In the two-tags model, one tag should be placed close to the transmitter and another should be placed close to the receiver. Lastly, it is noted that more than 5dB enhancement in effective SNR can be achieved by optimally locating the tags.

## I. INTRODUCTION

Backscatter communication is a hot technology to achieve the internet of thing (IoT) vision [1]. Visible light backscatter communication (VLC backscattering) has advantages on power efficiency [2], and it can use low-cost photo-diodes (PD) as a receiver without complex processing [3]. The location of tag is a important issue in the VLC backscattering, so this paper focused on optimizing the location of tags to maximize the effective signal to noise ratio (SNR).

#### A. Literature Review

Some prior studies showed that the network capacity of VLC backscattering can be increased by optimizing the reflection coefficient of tags [4]. The performance of SNR and interference between tags were studied in [5] and it gave the insight of optimizing both the location of tag and transmitter in each travel path, but it is a work for multiple tags and transmitters which contains more than ten tags and transmitters. The amount of energy harvested and reflected by the tag from the transmitter is the main index to determine a successful backscatter communication [6], [7]. The relationship among the communication distance, SNR, and bit error rate (BER) was indicated in [8] and [9]. They also indicated that deploying multiple-pixelated tags in VLC backscattering can increase the power harvested by the tag and overcome the single-channel power gain limitation. The SNR of VLC backscattering was improved by considering multiple-input multiple-output (MIMO) spatial diversity of tags in [9].

# B. Motivation and Contribution

VLC backscatter communication provides long-range, less interference, and more precise indoor communication [10]. The highly directional property facilitates a favorable sniffing function that correctly aligns the VLC system-guided optics with more precise positioning capabilities. At the same time, it also has no interference with ambient RF and electromagnetic waves which is an essential advantage in indoor communication [1], [2]. However, the optimization of tags has not been considered. We would like to address this gap because as noted from the literature on optimal relay placement [11], by optimally locating the tags, the corresponding VLC backscatter communication performance can be significantly enhanced. This paper fits that gap and our main contribution is four-fold. (1) Considering the single-tag VLC backscattering model, we show that the effective SNR at the receiver is a concave function of the location of the tag. Closed-form expressions of the optimal location were derived. (2) The novel expression of the sum of effective SNR is obtained under the practical constraint of blocking in the two tags model. (3) Joint concavity of this effective SNR in the two-tags model in terms of locations of two tags and effective transmitting time of each tag is proved. Closed-form expressions for the optimal location are also derived. (4) Numerical results have been provided to gain insights into tags' locations for different values of system parameters and showing achievable gains due to it.

# II. SYSTEM MODEL

# A. Adopted Topology for VLC Backscattering

In this paper, we consider both single-tag model and twotags model. The single-tag model of VLC backscattering comprises a transmitter, a tag and a receiver as shown in Fig. 1(a) below, whereas the four nodes topology comprises of one transmitter, two tags and one receiver as shown in Fig. 1(b) below. The locations of transmitter and receiver are fixed. Each tag is combined with an LCD shutter and a retroreflector.

# B. Channel Model for VLC Backscattering

1) Single-Tag Model: In Fig. 1(a), the distance between transmitter and receiver is labeled as D, and the distance between tag and receiver is labeled as d. Here m is the Lambertian order with  $m = -\frac{\ln 2}{\ln(\cos \varphi_{1/2})}$  where  $\varphi_{1/2}$  is the half power angle [12]. The channel power gain between transmitter and tag is donated as  $h_1$  and the channel power



Fig. 1: (a). The one tag model, (b). two tags model

gain between tag and receiver is defined as  $h_2$ . They are given by [13]:

$$h_1 = \frac{A_{tag}(m+1)g_x}{2\pi(D-d)^2}\cos^m\varphi\cos\epsilon,$$
(1)

$$h_2 = \frac{A_{PD}g_x}{2\pi d^2} \cos\phi\cos\theta,\tag{2}$$

In the Fig. 1(a), the  $\varphi$  is the angle of the irradiance respect to the transmitter vertically,  $\theta$  is the incidence angle of the receiver,  $\epsilon$  is the incidence angle of the tag, and  $\phi$  is the irradiance angle of the tag [14], [15]. The  $g_x$  is modulation index where  $g_x < 1$ .  $A_{tag}$  is the cross area of the square tag and and  $A_{PD}$  is the cross area of receiver.

2) *Two-Tags Model:* The channel power gains from transmitter to each tag at two-tags model are  $h_{d1}$  and  $h_{d2}$  [13].

$$h_{di} = \frac{A_{tagi}(m+1)g_x}{2\pi(D-d_i)^2}\cos^m\varphi_i\cos\epsilon_i, \forall i=1,2$$
(3)

where  $\varphi_i$  is the angles of the irradiance respect to the transmitter vertically,  $\theta_i$  is the incidence angles of the receiver,  $\epsilon_i$  is the incidence angle of the tags,  $\phi_i$  is the irradiance angle of the tags for all *i*=1,2 [14], [15].

From Fig. 1(a), s is the horizontal distance from tag to receiver (Rx). The distance from tag to Rx is labeled as d. In Fig. 1(a) we notice  $\phi$  is the reflection angle of  $\epsilon$ , so  $\phi = \epsilon$  and  $\cos \phi = \cos \epsilon = \frac{s}{d}$ . We also notice that  $\cos \theta = \frac{\sqrt{d^2 - s^2}}{d}$  and  $\cos \varphi = 1$  in Fig. 1(a) and we assume m = 1 here.  $\gamma_s$  can be defined as [1] [5]:

$$\gamma_s = \frac{2P_t L_m r A_{tag} A_{PD} g_x^2 \beta}{4\pi^2 \sigma^2 d^2 \left(D - \sqrt{d^2 - s^2}\right)^2} \left(\frac{s}{d}\right)^2 \left(\frac{\sqrt{d^2 - s^2}}{d}\right). \quad (4)$$

where  $L_m$  is the reflecting power loss after polarized, r is the photo-electronic conversion factor of the PD,  $\beta$  is the reflection coefficient.  $\sigma^2$  is the noise power.

# C. Bit Error Rate

The BER can be used to determine the quality of overall performance in the backscatter communication. The BER is a Q function of SNR ( $\gamma_s$ ) for VLC backscattering where Q function is a tail distribution function [13]. So the BER can be given by  $P_e = Q\left(\sqrt{\gamma_s}\right) = \frac{1}{\sqrt{2\pi}} \int_{\sqrt{\gamma_s}}^{\infty} e^{\frac{y^2}{2}} dy$  [8].

## **III. PROBLEM DEFINITION**

# A. Problem Definition for Single Tag Model

Our goal is to find optimal locations of tags to minimize BER. We present a preposition below that shares the key result.

Preposition1 : Minimization of  $P_e$  can be achieved by maximizing  $\gamma_s$ .

**Proof** : The Q function is monotonically decreasing, thus, the minimization of  $P_e$  is equivalent to the maximization of  $\gamma_s$ .

The corresponding optimization problem (P1) is given as:

(P1): maximize 
$$\gamma_s$$
  
subject to  $C1: d < D, C2: d > \delta_0.$  (5)

Here  $\delta_0$  is the minimum distance between any two nodes to be in the radiating far-field region [11].

## B. Optimisation Formulation for Two Tags

In the two-tags model, the objective is to maximize the sum of effective SNRs. Since we assume that two tags are working at different times, so we define C as duty cycle which denote the time for which the first tag  $T_1$  is transmitting. Also it needs to noticed that if there are two tags,  $T_1$  is going to block the energy from Tx to  $T_2$ , where the block power is donated as  $P_{block1}$ . Whereas the  $T_2$  will block the backscattering from  $T_1$ to Rx and, its block power is donated as  $P_{block2}$  [16]. These blocking powers are respectively defined below:

$$P_{block1} = A_{tag2}^2 \frac{P_t (m+1)^2 g_x^2}{16\pi^2 d_2^3 (D-d_1)^2} \frac{\lambda \Delta_1}{d_1 + d_2}.$$
 (6)

where  $\Delta_1 = \cos^m \varphi_2 \cos \epsilon_2 \cos \phi_2 \cos \theta_2$  and  $A_{tag2}$  is the cross-section area of  $T_2$ .

$$P_{block2} = A_{tag1}^2 \frac{P_t (m+1)^2 g_x^2}{16\pi^3 d_1^2 (D-d_2)^2} \frac{\lambda \Delta_0}{d_1 + d_2}$$
(7)

where  $\Delta_0 = \cos^m \varphi_1 \cos \epsilon_1 \cos \phi_1 \cos \theta_1$ .  $\lambda$  is the wavelength of the light emitted from Tx.  $A_{tag1}$  is the cross-section area of  $T_1$ .  $P_{tag1}$  below is the energy receiver at  $T_1$  and  $P_{tag2}$  is the energy receiver at  $T_2$  [5]:

$$P_{tag1} = \frac{CP_t A_{tag1} g_x^2 (m+1) d_1 \cos^m \varphi_1 \cos \epsilon_1}{2\pi (D-d_1)^2}.$$
 (8)

$$P_{tag2} = (1 - C) \frac{P_t A_{tag2} g_x^2 (m+1) d_2}{2\pi (D - d_2)^2} \cos^m \varphi_2 \cos \epsilon_2.$$
(9)

Thus, The sum of effective SNR  $(\gamma_{s2})$  of two tags model returned as:

$$\gamma_{s2} = \frac{P_{tag1} - P_{block1} + P_{tag2} - P_{block2}}{\sigma^2}.$$
 (10)

where  $\sigma^2$  is the noise. Since we objective is to maximize the sum of effective SNR by optimisation of location of tags, the corresponding optimization problem (P2) is given:

$$(P2): \underset{d_1,d_2,C}{\operatorname{maximize}} \quad \gamma_{s2}$$
  
subject to  $C3: D \ge d_1 \ge \delta_0, \quad C4: d_2 \ge d_1 + \delta_0, \quad (11)$   
 $C5: d_2 \le D, \quad C6: 0 \le C \le 1.$ 

#### IV. OPTIMAL LOCATION FOR SINGLE TAG MODEL

In this section, we will discuss the optimization problem P1. Firstly we will check the convexity of the objective function.

# A. Convexity Check

We find second derivative of  $\gamma_s$  to check convexity. As  $\frac{\partial^2 \gamma_s}{\partial d^2} = -1.25(ds/D - 0.23)^3$ , the  $\frac{\partial^2 \gamma_s}{\partial d^2}$  of the objective function in (4) is positive when ds/D < 0.23 and is negative when  $d > \frac{0.23}{s}D$ , so, the function  $\gamma_s$  is concave when  $d > \frac{0.23}{s}D$ .

## B. Optimal location

The SNR defined in (4) is concave when  $d > \frac{0.23}{s}D$ , we show that only one solution as obtained by solving  $\frac{\partial \gamma_s}{\partial d} = 0$  lies on that region. After solving  $\frac{\partial \gamma_s}{\partial d} = 0$ , we obtain  $d = \sqrt{-\frac{1}{3a}(b + \frac{\kappa}{\xi} + \xi)}$ , and we notice that there are six solutions according to six different values of  $\xi$ . Here a = 36,  $b = -(96s^2 - 16D^2)$  and  $\kappa = 36s^4 - 256D^4 - 4320D^2s^2$ . Those six solutions of  $\gamma_s$  contains three imaginary numbers and only for  $\xi = 1, 0.2s^2$  and  $152s^2$ , the solutions will be real. d < 0 when  $\xi = 1$ .  $d > \frac{0.23}{s}D$  when  $\xi = 152s^2$  which is optimal value on the range of concave and when  $\xi = 0.2s^2$  the solution is convex which is minimum. So we do not consider  $\xi = 0.2s^2$  case and the optimal location for single tag is given by:

$$d^* = \sqrt{\frac{56s^2 - 16D^2}{108} + \frac{36s^4 - 256D^4 - 4320D^2s^2}{152s^2}} \quad (12)$$

**Remark 1.** The globally optimal location for single tag is given by  $d^*$  in (12) because  $d^*$  lies in the concave region, and other feasible roots lie in the convex region.  $d^*$  is always larger than  $\delta_0$  and smaller than D which satisfies C1 and C2.

# V. OPTIMAL LOCATION FOR TWO TAGS MODEL

In this section, we investigates the optimization problem P2. We start checking the joint convexity of  $\gamma_{s2}$  with respect to  $d_1$ ,  $d_2$  and duty cycle C. Next, we obtained optimal location of given C follow by optimal C for given locations. Lastly, we find joint optimization in closed-form.

# A. Convexity Check

To check the convexity of optimization problem P2, we firstly prove the concavity of  $\gamma_{s2}$  by observing Hessian Matrix and its determinant which are defined below:

$$\nabla^{2}\gamma_{s2} = \begin{bmatrix} \sqrt{d_{1}^{3}} - d_{1}^{3} & \frac{(D-d_{1})-2d_{1}+1}{(D-d_{1})^{3}} & \frac{1}{(1-C)(d_{1}+d_{2})^{2}} \\ \frac{(D-d_{1})-2d+1}{(D-d_{1})^{3}} & d_{1}^{\frac{3}{2}} - d_{2}^{\frac{3}{2}} & 0 \\ \frac{1}{(1-C)(d_{1}+d_{2})^{2}} & 0 & \frac{d_{1}-d_{2}}{(d_{2}+d_{1})^{3}} \end{bmatrix}$$
(13)

$$\det(\nabla^2 \gamma_{s2}) = \frac{(D-d_1)(d_1+2d_1)\sqrt{d_1d_2}}{(1-C)^2(d_1-d_2)(D-d_1-d_2)^2} < 0.$$
(14)

The determinant of this Hessian Matrix  $(\nabla^2 \gamma_{s2})$  is given by (14) that is negative because  $d_1 - d_2 < 0$  under C4. Meanwhile, the three principal minors  $d_1^{\frac{3}{2}} - d_1^3$ ,  $\frac{d_1 - d_2}{(d_2 + d_1)^3}$ , and  $d_1^{\frac{3}{2}} - d_2^{\frac{3}{2}}$  in the 1×1 matrix are all less than zero, and the principal minors of 2×2 matrix,  $d_1 d_2 \sqrt{d_1 d_2} + (\frac{(D-d_1)-2d_1+1}{(D-d_1)^3})^2$  and  $\frac{(d_1 - d_2)(d_1^{\frac{3}{2}} - d_2^{\frac{3}{2}})}{(d_2 + d_1)^3}$  are both larger than zero. So the  $\gamma_{s2}$  is jointly concave in  $d_1$ ,  $d_2$  and C along with the linear constraints C3, C4, C5 and C6.

# B. Location Optimization

In this section, we find optimal location for a given duty cycle. The objective function is jointly concave so we can find optimal solution by taking derivative for  $d_1$  and  $d_2$  respectively and set them to zero. We start with derivative of  $d_1$ . We get four solutions after solving  $\frac{\partial \gamma_{s2}}{\partial d_1} = 0$ . Under C3 of P2, only one solution is feasible.

$$d_1 = \sqrt{\frac{2DC^2(D^2 - 1.35Dd_2 + DCd_2)}{25(D - d_2)^2(1 - C)}}.$$
 (15)

Then, we take derivative for  $d_2$  and have  $\frac{\partial \gamma_{s2}}{\partial d_2} = 0$ . It is a quadratic functions with two solutions. But one solution is smaller than  $d_1$  which is non-feasible under C4, thus, the feasible solution is given below:

$$d_2 = \frac{D(1-C)}{3C} + 0.525d_1. \tag{16}$$

We substitute (16) into (15) and find the optimal  $\hat{d}_1$  which is given by:

$$\widehat{d}_1 = \frac{0.475D + 0.32DC^3 + \sqrt{2.25D^2 + 1.29D + 0.56}}{0.95(1 - C)}.$$
 (17)

Next to find the optimal location  $\hat{d}_2$  we need to substitute (17) into (16) and obtain following result:

$$\widehat{d}_{2} = \frac{0.5D + 0.3DC^{3} + \sqrt{2.25D^{2} + 1.3D + 0.56}}{0.6(1 - C)} + \frac{D(1 - C)}{3C}.$$
(18)

# C. Duty Cycle Optimization

Here we need to find optimal duty circle C for given locations  $d_1$  and  $d_2$ . We need to substitute the  $d_1$  and  $d_2$  into equation (10) so there will obtain an objective function only in term of C and set  $\frac{\partial \gamma_{s2}}{\partial C} = 0$ . We observe the first derivative of  $\gamma_{s2}$  is a quadratic equation which has two solutions. However, under the constrain C6 in P2, one solution of C will be smaller than 1. Thus, the optimal duty cycle for given  $d_1$  and  $d_2$  is given by:

$$\widehat{C} = \frac{24D^2d_1}{15.38d_2} + \frac{(1.48d_2^2D^2 - 0.7D^2)^2}{15.38d_2\sqrt{2.25D^2 + 1.29D + 0.56}}.$$
 (19)

# D. Joint Optimization

Here we investigate the joint optimization of  $d_1^*, d_2^*$  and  $C^*$ . To achieve this, we firstly need to substitute optimal  $\hat{C}$  as obtained in (19) into (17) and (18). After substituting  $\hat{C}$ , we get two quadratic equations in  $d_1$  and  $d_2$  respectively. On solving  $d_1$  and  $d_2$  respectively, we obtain jointly optimal solution of  $d_1^*$  and  $d_2^*$  respectively which are shown below where satisfy the C3, C4, and C5:

$$d_1^* = \frac{0.3D^2 + D^3 + 0.5D^4 + \sqrt{2.25D^2 + 1.29D + 0.56}}{0.13D + 0.06D^3 + 1.5D^2}.$$
(20)

$$d_2^* = d_1^* + \frac{D+7}{D^2 - 7.12D}.$$
(21)

In the end, we need to substitute (20) and (21) into (19) to get the joint optimal duty cycle  $C^*$  which is shown below:

$$C^* = \frac{\sqrt[3]{(0.56D - 14.12D^2 + 2.28D^3)}\sqrt{D(1.23 + 5.87D)}}{4.5D\sqrt{(2.25D^2 + 1.29D + 0.56)}} + \frac{27.54D}{D^2\sqrt{D} - 4.5D^2}.$$
(22)

## VI. NUMERICAL RESULTS AND CONCLUSION

The value of D is set as 100m. The areas of square tags and receiver are  $0.4\text{m}^2.\beta$  and  $L_m$  are both 0.5. The optoelectronic conversion factor of the PD, r is 0.7 with a fixed noise variance  $\sigma^2 = 30$  [5]. The illumination power of each Tx  $P_t = 10$ W.

A. Single Tag Model



Fig. 2: The relationship of BER and SNR with distance "d"

Fig. 2 above plots SNR and BER as a function of d for different values of s to verify Preposition 1 that maximizing

SNR is equivalent to minimizing BER. It indicates that the BER will always be minimized when the tag is closer to the transmitter. It also shows that when *s* is increased, the location of the tag will be farther from the transmitter so BER increases. The numerical results show that the optimized location of the tag should be closer to the transmitter compared to receiver.



Fig. 3: The optimal d versus different value of D and s

Next we investigate the insights of optimal tag's location on the different s and D. As showing in Fig. 3, the optimal location of tag moves towards to receiver initially but after a certain distant that are 870m it again close to the transmitter.

## B. Two Tags Model

In the two tags model we aim to investigate how the effective SNR depends on three variables:  $d_1$ ,  $d_2$  and C. Specifically, we plot the optimal duty cycle as obtained in



Fig. 4: The optimal C versus different location of tags

(19) as the function of  $d_1$  and  $d_2$  in Fig. 4. It indicates when tags are far away from transmitter  $T_1$  is given less time to work and when tags are near  $T_1$  needs to be given more time. Specifically, when the location of  $T_1$  between the value of 0.2D and 0.4D it is given most time, otherwise, when  $T_1$  is either very near the transmitter or very far from transmitter,  $T_2$  need to be given more time.

Now we shift to show the relation of maximum effective SNR, optimal  $\hat{d}_1$  and  $\hat{d}_2$  for different value of C and D. In Fig. 5(*a*), 5(*b*) and 5(*c*) we respectively show the maximum effective SNR and optimal location  $\hat{d}_1$ ,  $\hat{d}_2$  for different values of C and D.

**Remark 2.** Two-tags model with low D in Fig. 5, maximum SNR is achieved for  $\frac{d_1}{D} = 0.3$ ,  $\frac{d_2}{D} = 0.7$  and C = 0.25. SNR



Fig. 5: (a) Effective SNR, (b) optimal location  $\hat{d}_1$ , and (c) optimal location  $\hat{d}_2$  for different values of C.

increases when  $d_1$ ,  $d_2$  and C are increasing until  $\frac{d_1}{D} = 0.3$ ,  $\frac{d_2}{D} = 0.7$  and C = 0.25, then SNR decreases again.

#### C. Comparison

Here we come to compare the BER of optimal location for two values of s against three fixed locations which are (1) close to the transmitter, (2) close to the receiver, and (3) at the center. In Fig. 6, the location at the center is better than at the sides and the BER is increasing when s is increasing. The BER at optimal d is 45% lower than it at center when s = 0.2D and 41% lower when s = 0.8D.



Fig. 6: BER for different values of d in single tag case



Fig. 7: Comparison of fixed location, optimal duty cycle, optimal location and joint optimization

For the two-tags model, we compare the jointly optimization of location and duty cycle  $d_1^*$ ,  $d_2^*$  and  $C^*$  against three fixed allocation schemes on different value of D: (a). fixed  $d_1 = 0.5D$ ,  $d_2 = 0.6D$  and C = 0.5, (b). optimal  $\hat{C}$ ,  $d_1 = 0.5D$  and  $d_2 = 0.6D$ , and (c). optimal  $\hat{d}_1$  and  $\hat{d}_2$ while C = 0.5. From Fig. 7, the gain improvement by optimal duty cycle, optimal locations and joint optimal schemes over fixed allocation scheme are respectively around 0.6dB, 4.2dB, and 6.4dB when D = 100m and around 0.1dB, 5.91dB, and 8.98dB when D = 500m. Also the gain improvement by optimal duty cycle, optimal locations and joint optimal schemes over fixed allocation scheme are around 0.22dB, 0.9dB, and 5.56dB when D = 1000m. However, when D = 2000m there is no significant improvement by optimal duty cycle and optimal locations over fixed location, only the joint optimal scheme improves around 4.26dB over other semi-adaptive schemes. Fig. 7 indicates that the SNR of joint optimization is always better than the semi-adaptive schemes and the SNR decreases when D increases.

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